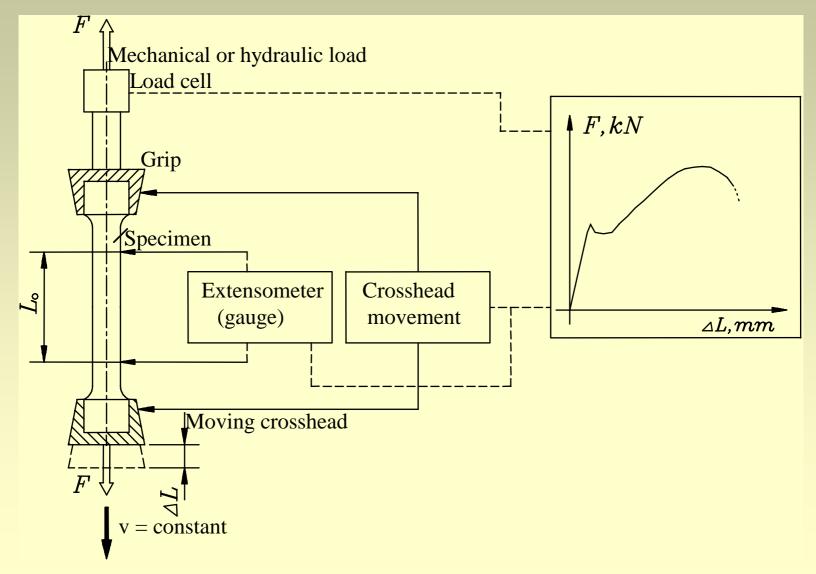
Mechanical Testing 1

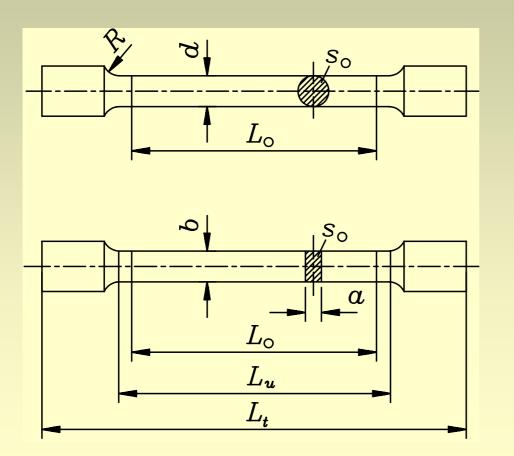
to determine if the material meets specification
to establish design parameters
to evaluate the effects of processing variables

1

Tensile (tension) test



Tensile specimen



General geometry

 $L_O = 5 \cdot d_O$

 $L_0 = 10 \cdot d_0$

Tensile specimens



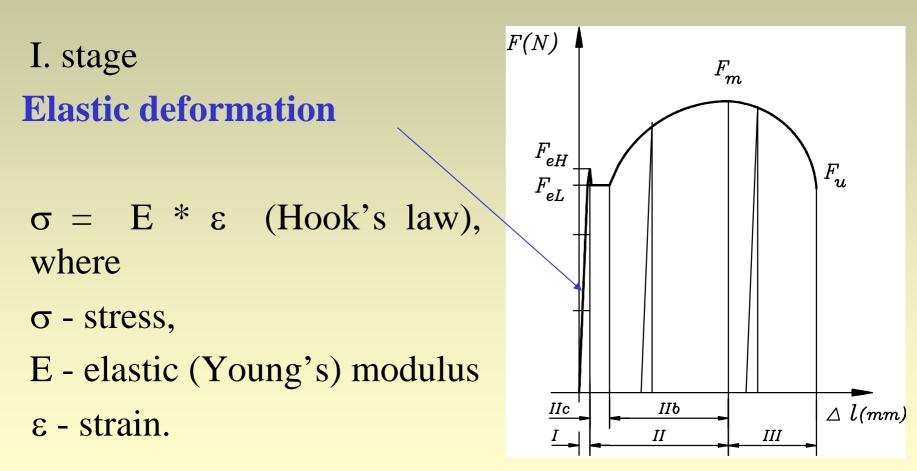




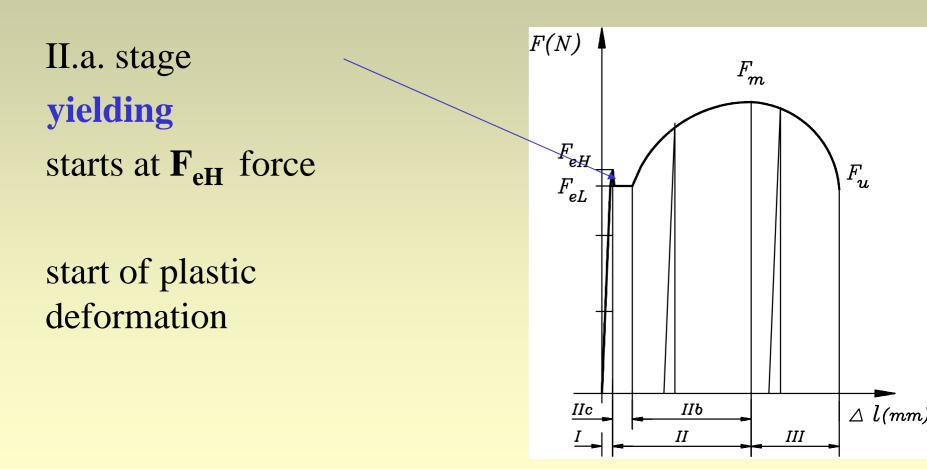




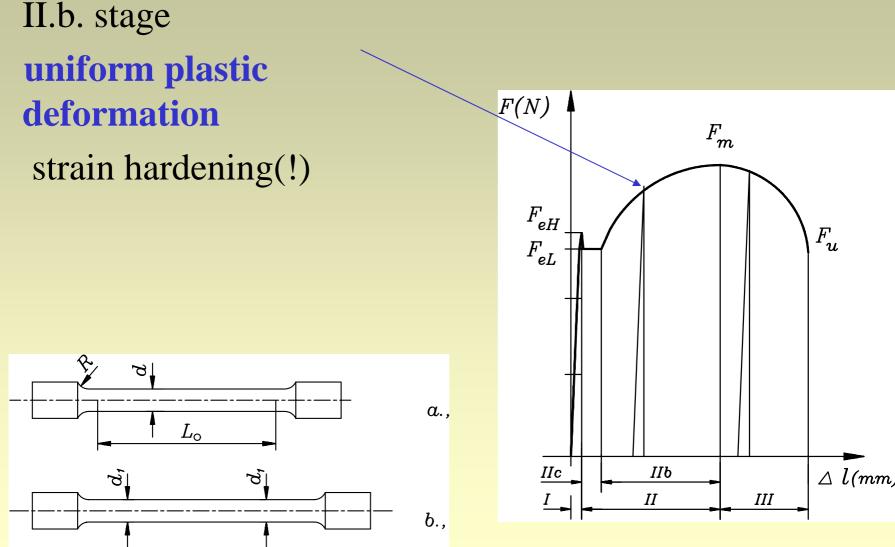
Tensile diagram (1)



Tensile diagram (2)



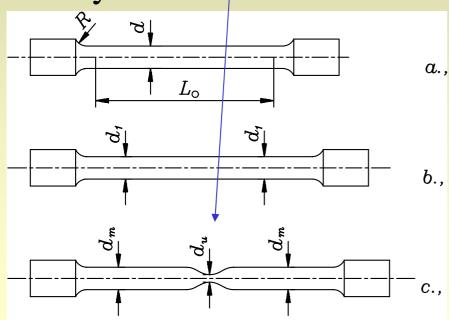
Tensile diagram (3)

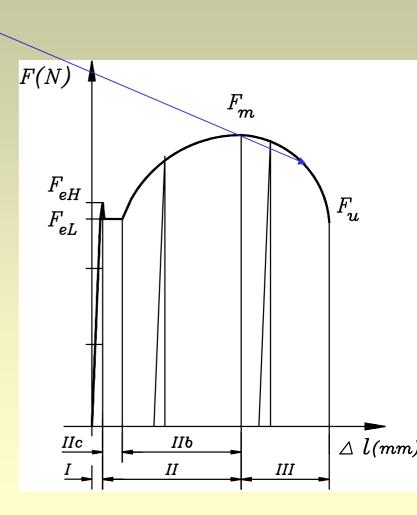


Tensile diagram (4)

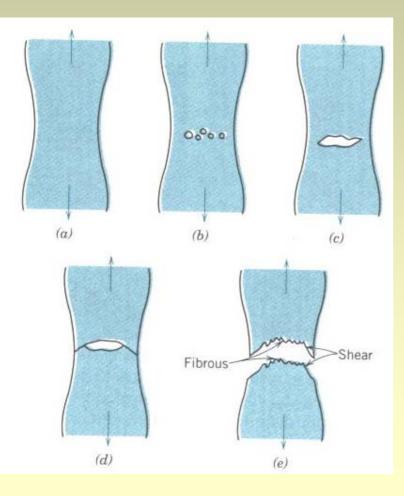
III. stage Necking

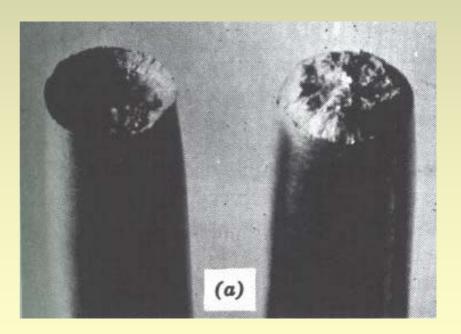
the strain becomes localised to a small volume only





The process of rupture





Calculation of material properties: Engineering system Force and elongation is divided with the original cross section and gauge length $\sigma = F/S_{o}$ stress : strain, specific elongation : $\varepsilon = \Delta L/L_o$ where F - force S_o – original cross section L_o – original gauge length ΔL – length difference

Calculation of material properties: Real system

Force and elongation is divided with the **<u>actual</u>** cross section and gauge length

stress:
$$\sigma' = \frac{F}{S}$$
 $d\phi = \frac{dL}{L}$
integrating the equation: $\varphi = 2\ln \frac{L_0}{L}$

F – force

S- actual cross section

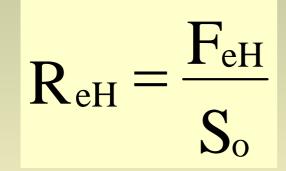
dL – actual length difference

 d_o – original diameter

d- actual diameter

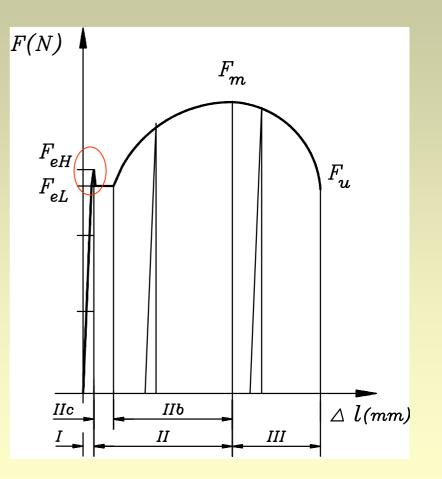
 φ – logarithmic strain

Material properties: Yield strength



Stress at yielding

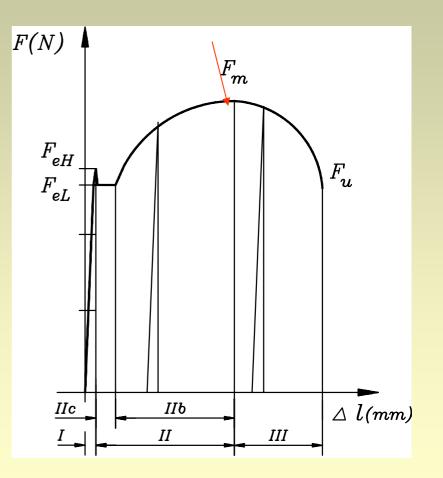
N/mm²



Material properties: Tensile strength

$$R_{\rm m} = \frac{F_{\rm m}}{S_{\rm o}}$$

Ultimate tensile strength (UTS or TS) is a measure of the maximum load that a material can whitstand. N/mm²



Material properties: Measure of ductility

• Elongation, A

% change in length/initial length

$$A = \frac{L_u - L_o}{L_o} 100 \%$$



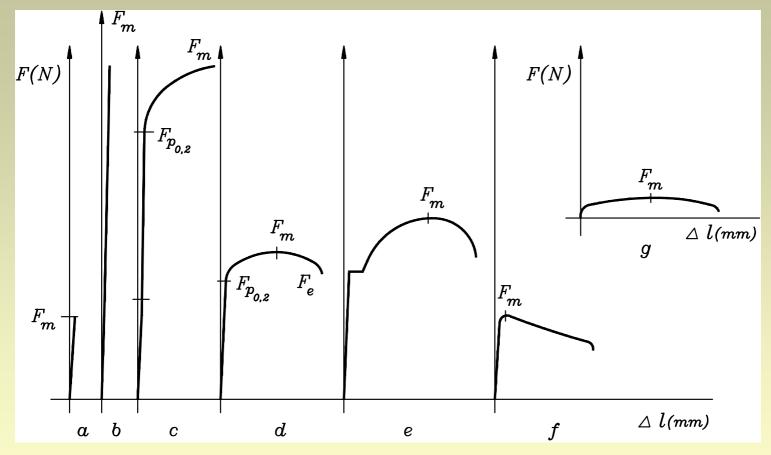
Material properties: Measure of ductility

 Reduction in area, Z
 %
 change in cross section/initial cross section

$$Z = \frac{S_o - S_u}{S_o} 100\%$$



Yield strength – Proof strength



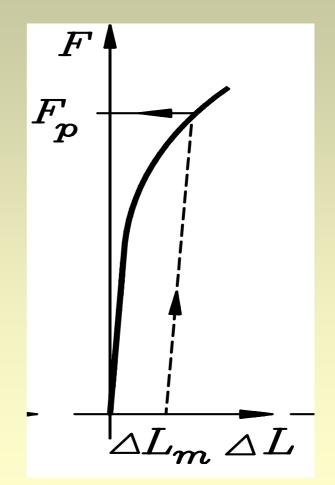
If characteristic yielding can not be observed, we calculate proof stress as: **stress at a given elongation** (e.g. 0,2%)

Proof strength

Stress required to produce a small amount of plastic deformation :

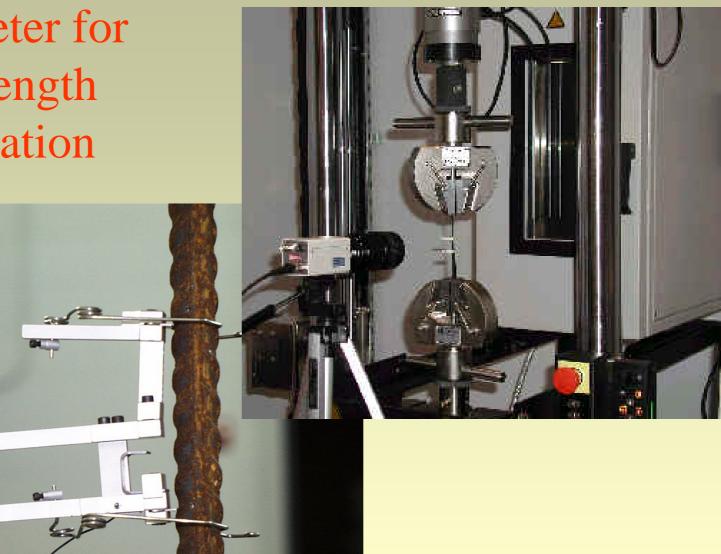
$$R_{p0,2} = \frac{F_{p0,2}}{S_o}$$
 [N/mm²]

specified value of strain offset: usually 0,2 % of gauge length



Extensometer for proof strength determination

634.12E-24



Tensile test machine

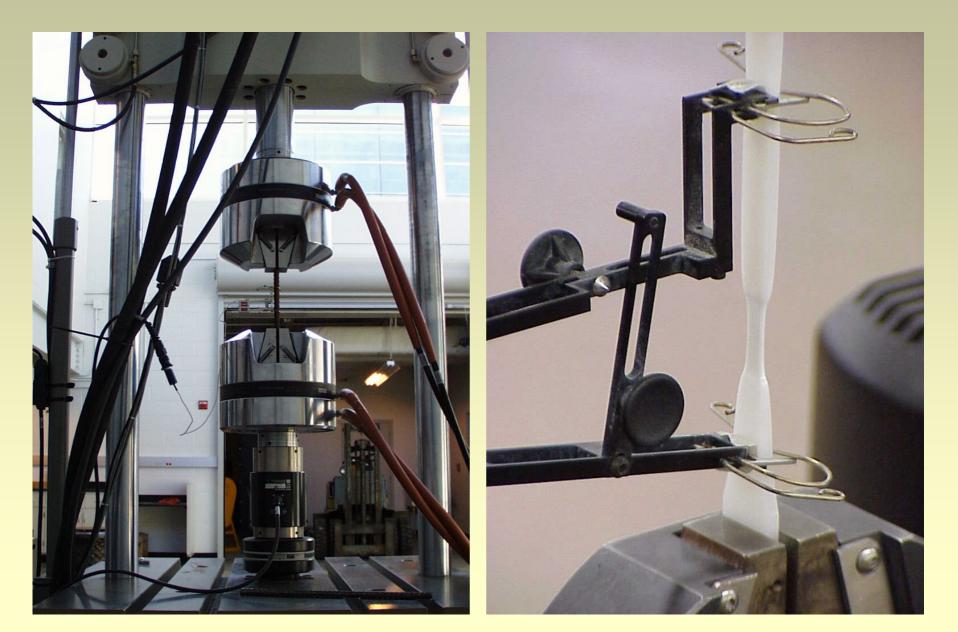
Load capacity: 100 kN

Elongation measurement with optical extensometer

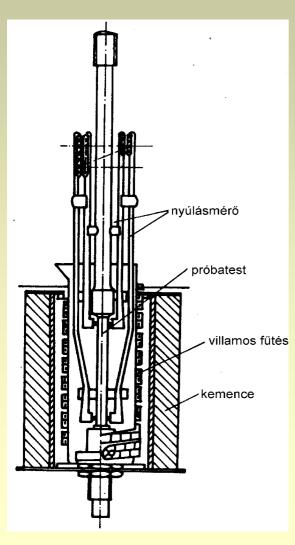
Automated evaluation of stress, strain, anisotropy, etc.

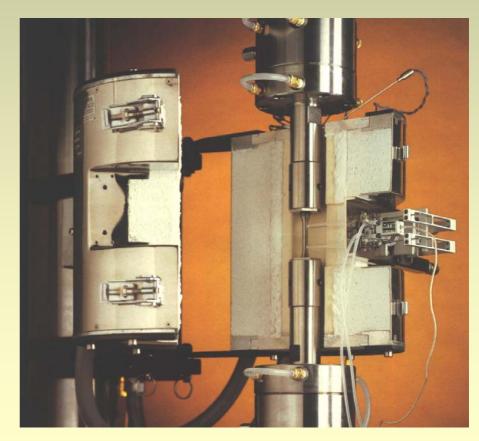


Tensile test machine: testing of polymers

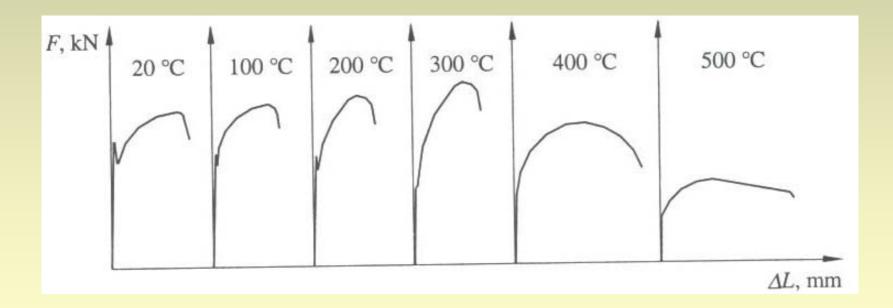


Tensile test at elevated temperature





Tensile diagrams of steel at elevated temperatures



Factors affecting the results of tensile test

specimen geometry, surface roughness

the rate of increase of load

testing conditions, ie. temperature

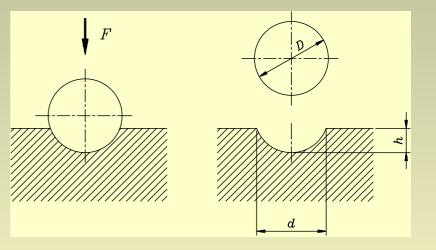
Hardness test

simple, short time ,,non-destructive" charaterises the mechanical parameters fits to the technological line

- Indentation hardness tests (Brinell, Vickers, Rockwell)
- Rebound or dynamic tests

Brinell hardness test

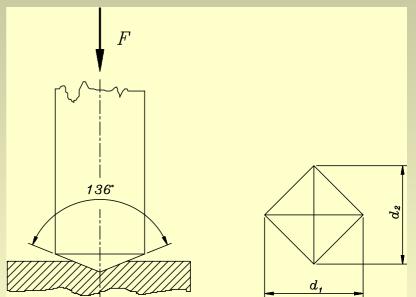
- Ratio of force (F) and the surface of indentation (A)
- Indentor: steel or tungsten carbide ball
- HB, depends on the force and on the ball diameter!
- No unit of measure!
- Standardized, table
- Used for castings, forgings, heavy sections



 $HB = \frac{0,102 \cdot F}{A} = \frac{0,102 \cdot 2F}{D\pi \left(D - \sqrt{D^2 - d^2}\right)}$

Vickers hardness test

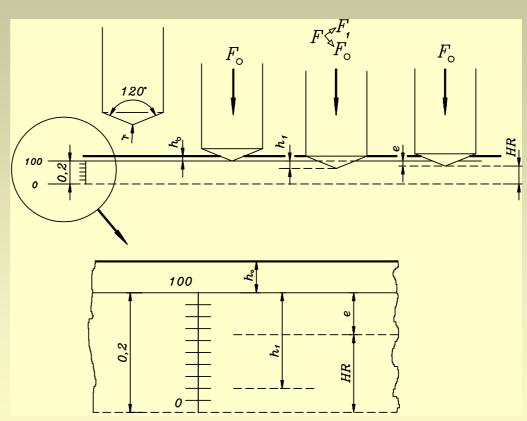
- Ratio of force and the surface of indentation
- Indentor: diamond pyramid
- HV, more or less undependent on the force, No unit of measure!
- Standardized, table evaluation
- Used for accurate measuring, hardness distribution, microhardness!



 $HV = 0,102 \cdot 1,854 \cdot \frac{F}{d^2}$

Rockwell hardness test

- diamond cone
- pre-load
- main-load
- pre-load
- HRC depth of indentation



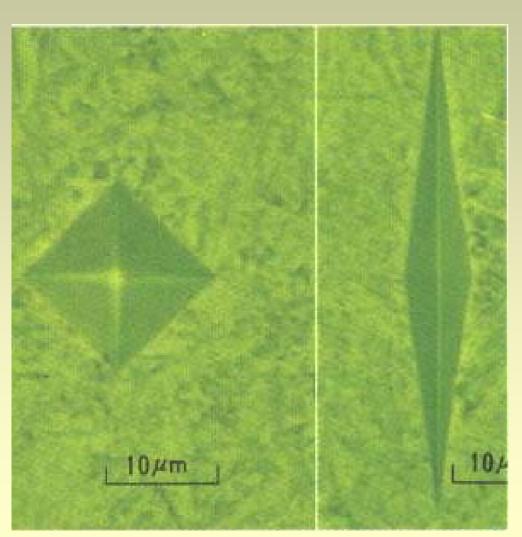
 $HRC = 100 - (h_1 - h_0)/0,002$

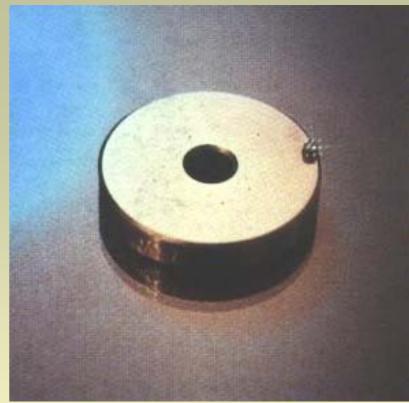
Példa: h_1 - h_0 =0,08 mm => HRC = 100 - 0,08/0,002 = 60







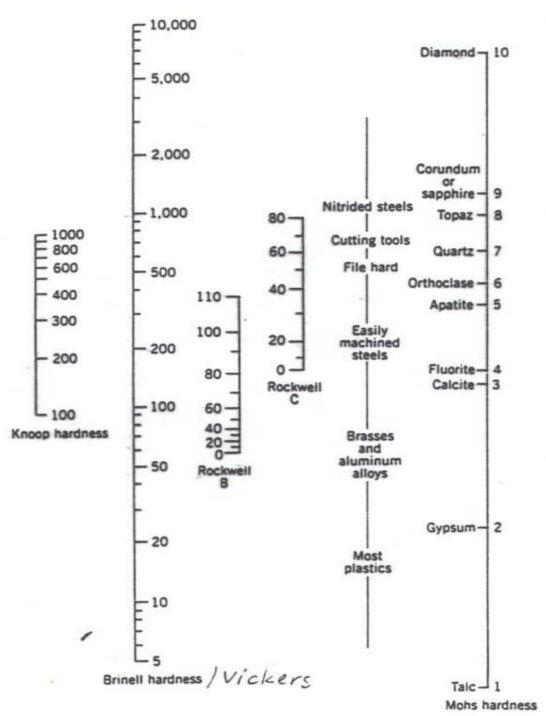




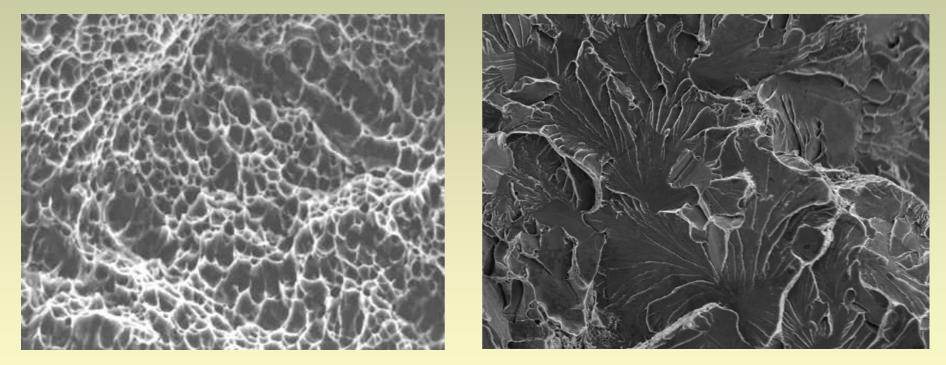
Rebound hardness test



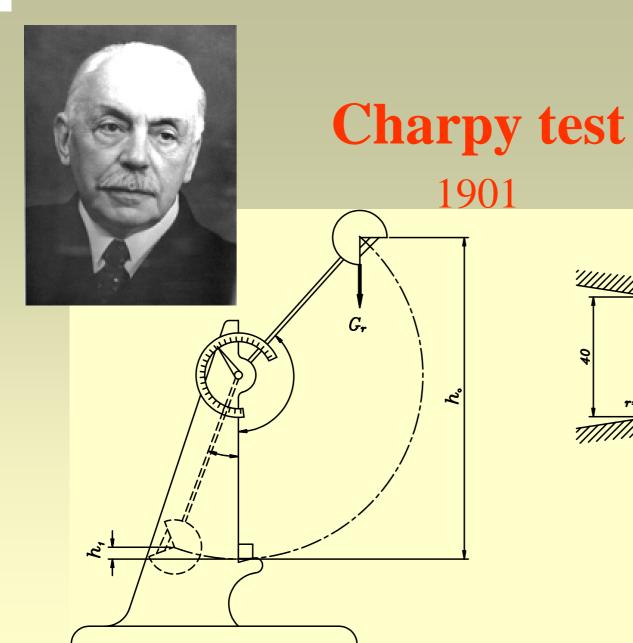
Comparison of hardness scales



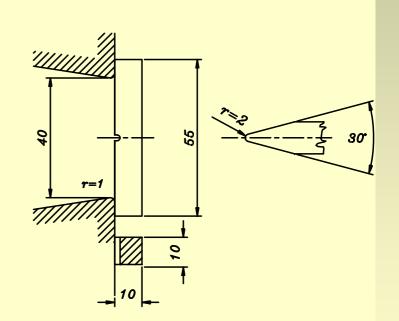
TOUGH - BRITTLE behaviour



Difference: - plastic deformation --absorbed energy

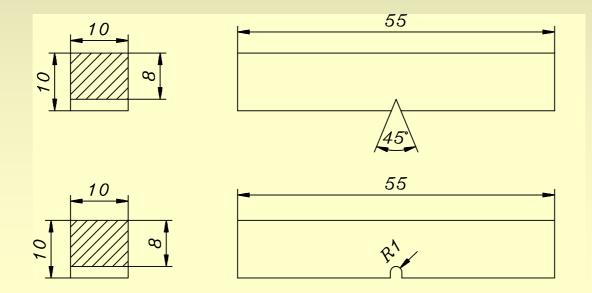


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Charpy specimen

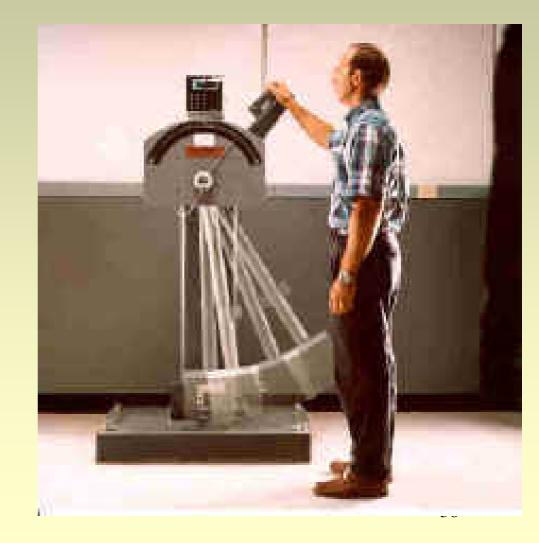
The sizes of the specimen are: 10x10x55 mm with a 2 mm deep V or U shaped notch



Charpy test

The energy absorbed by the fracture can be calculated as follows:

 $\mathbf{K} = \mathbf{G}_{\mathbf{r}}(\mathbf{h}_{\mathbf{o}} - \mathbf{h}_{1}) [\mathbf{J}]$



Factors influencing ductile/brittle behaviour

- Temperature
- The speed of deformation
- The stress state





The phenomenon of creep

Crrep is a slow, continuous deformation with time under constant load: the strain instead of depending only on stress, now depends also on time and temperature. At elevated temperatures the creep can accelerate, ending in fracture.

T > (0,3...0,4) T_m (K), for metals T > (0,4...0,5) T_{me} (K), for ceramics

Stress, temperature and time

The creep behaviour is well understood in general, that is the higher is the temperature and the higher is the stress, the greater is the creep rate and the shorter is the time to fracture. The complete quantitative description of the creep process is lenghty and complex..

Stress, temperature and time

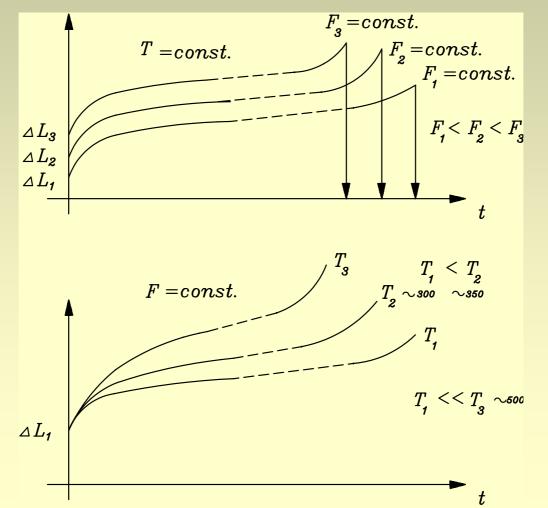
Creep behaviour is best characterised by creep curves.

Creep curves can be determined by applying constant load on specimens heated in resistance furnaces. The furnaces are equipped with extensometer so the strain versus time valuaes can be plotted.

Creep curves have three distinctive parts.



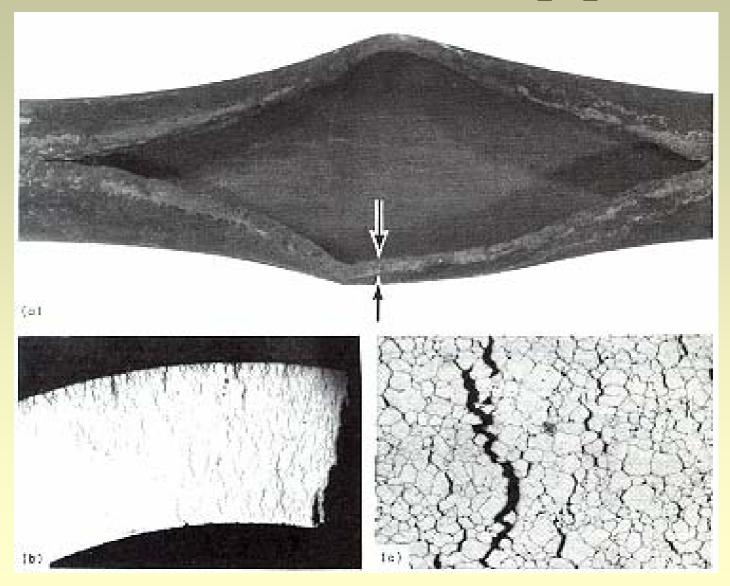
The effect of stress and temperature on creep



43



Fracture of a boiler pipe.



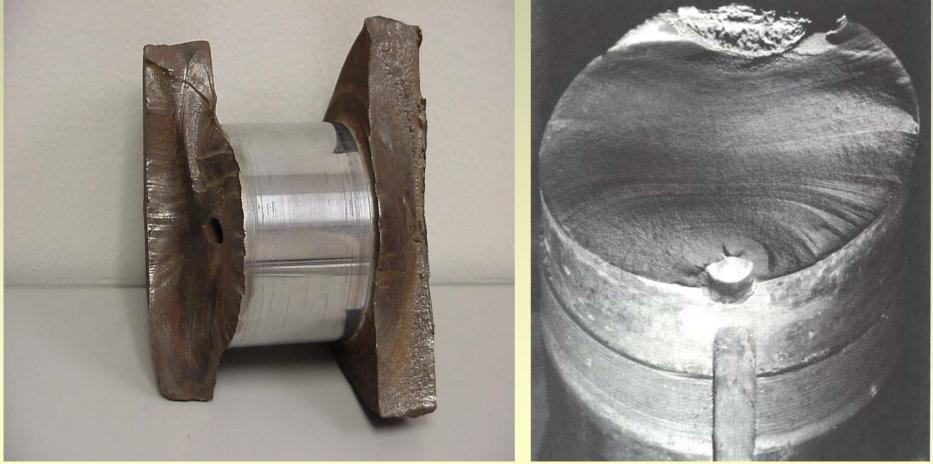


The fatigue phenomenon

If a component is subjected to repeated stress cycles, like the loading on a connecting rod of an engine or on the wing of an aircraft, it may fail at stresses far below the yield strength of the material. This phenomenon is called fatigue.

The fatigue fracture surface has a characteristic clamshell pattern.

Characteristics of the fatigue fracture surface



The process of fatigue

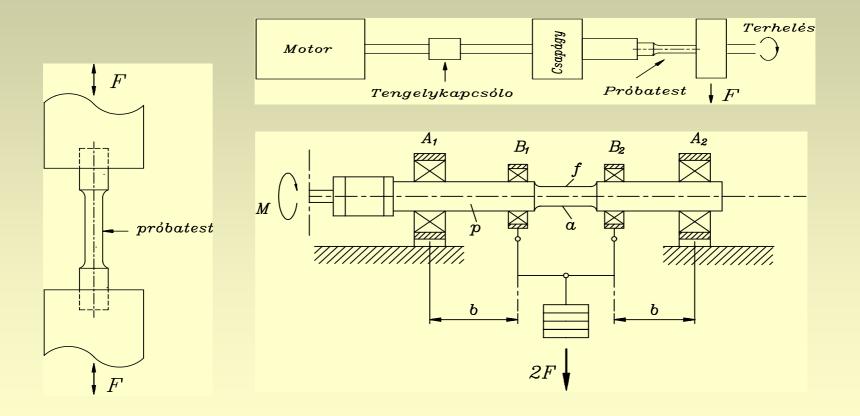
 $\sigma < R_{\rm p0,2}$

- There is no macroscopic plastic deformation,
- but on microscopic level plastic deformation may occur, because enginnering materials are:
- not homogenous and they are anizotropic
- the orientation of crystallites are diffrent
- there are inclusions and flaws in the material

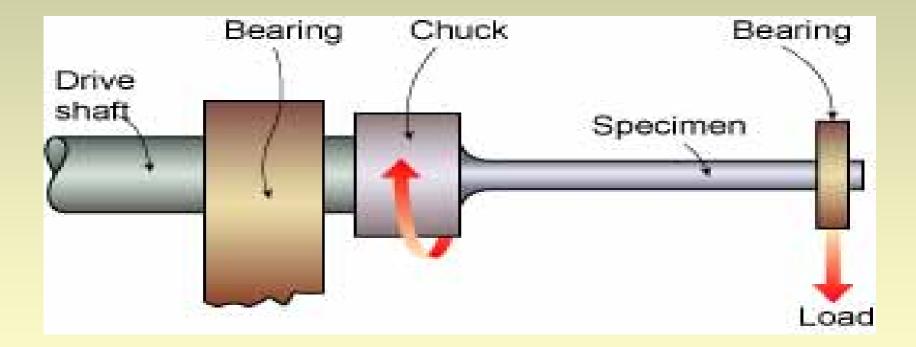
August Wöhler, 1858



Arrangement of fatigue tests



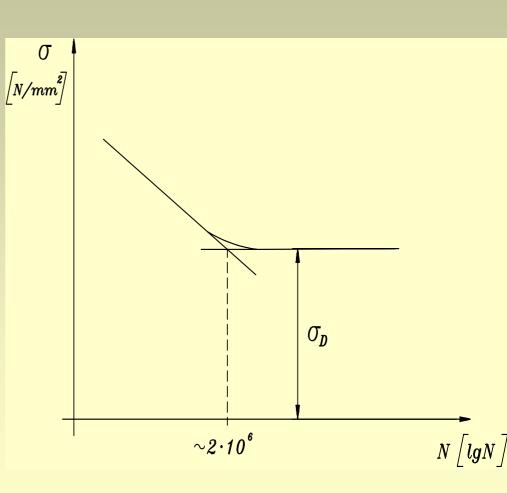
Arrangement of the rotary-beam fatigue test



In case of steels the curve approaches a stress value in assimptotic way

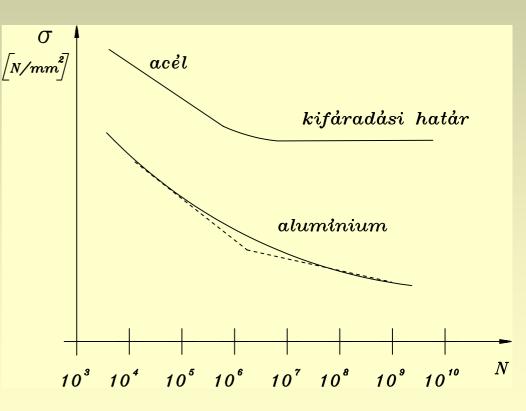
Gradually reducing the load a characteristic stress can be determined that could be applied infinitive times without causing fracture. This value is the fatigue limit, also called endurance limit.

Wöhler diagram



Not every material has fatigue limit

In case of Al-alloys, stainless steels, high strength steels the second part of the Wöhler diagram is not horizontal, these materials do not have fatigue limit.

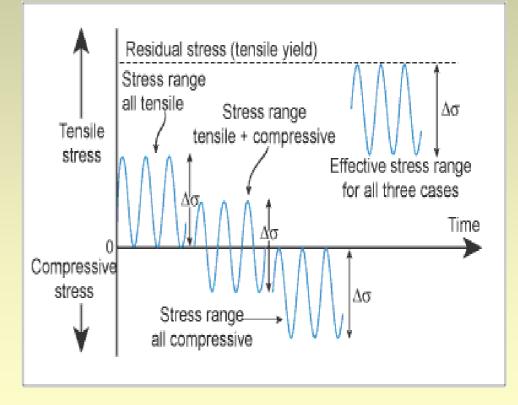


Fatigue behaviour of nonmetallic materials

- The fatigue behaviour of polymers is similar to that of the metals, although the microscopic process is different in them.
- Ceramics are brittle, they do not exhibit fatigue behaviour

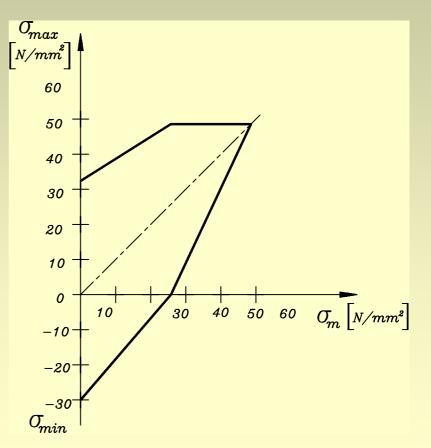
The variation of stress with time

Under cyclic load the stress varies with time sinusoidally either in swinging or pulsating way. The stress may be characterised its medium, maximum and minimum value.



Safety area Smith-diagram

In the Smith diagram the maximum and minimum stresses belonging to a given number of cycles are plotted against the medium stress.



Factors influencing the fatigue behaviour

Many factors affects the data of the fatigue test, such as:

- the type of load
- design
- microstructure
- environment
- surface finish and treatment

F/A -18 Full Scale Fatigue Test

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